	DESIGN C	F BEAM-	COLUMNS	SC	also see the ac	companying di	scussion				
		Ŀ	BEAMCOL	C							
Example Problem 1.	See Figure	2. Eccen	ntric load =	1000 pound	ds. Major axis e	= 1.0", minor a	xis e = .5"			Engineering F	rope
Job	Major axi	s side unit	form load r	noment =80	00 lb-ft, minor ax	is side load mo	oment = 200 lt	o-ft.			· ·
Notes	Full 3"x6"	length =	96", with i	ntermediate	weak axis braci	ng at 2'-8" o.c.				(grade)	
	Normal Ic	ads and c	conditions	No. 2	Doug Fir-Larch	Check a	adequacy			Doug Fir-Larch	1,
Cill in confluence and the balance										Eastern Hemlock	1,
Fill In yellow cells below				بينوالون وطفر	aalla thia	Load Duration F	actors,C <sub>D</sub>			Hem-Fir	1,
Light green cells are tables		-	enreadeb	ent is protec	ted to prevent	permanent		0.9		Hem-Fir (north)	1,
Light groot bollo are tabled			accidenta	I loss of the	formulas	snow		1.15		Redwood	1,
LOAD DESCRIPTION						construction		1.25		South'n Pine	1,
Major axis moment due to side	load A =	800	lb-ft			wind, quake		1.6		Spruce,Pine,Fir	1,
Minor axis moment due to side	load B=	200	lb-ft							Westn Cedar	1,
Axial (column) load =		1000	pounds								
Major axis eccentricity $(e_1) =$		1.00	inches							Engineering	Prop
Minor axis eccentricity (e <sub>2</sub> ) =		0.50	inches							Posts & Timbers	
STRESS ADJUSTMENT FACTO	ORS									(grade)	
load duration factor, C <sub>D</sub>		1.00			Temperature Fa	ctors,Ct	•			Doug Fir-Larch	
size factor, C <sub>F</sub> for bending		1.30			M.C.	100 <t 125<="" td=""><td>125<t 150<="" td=""><td></td><td></td><td>Eastern Hemlock</td><td></td></t></td></t>	125 <t 150<="" td=""><td></td><td></td><td>Eastern Hemlock</td><td></td></t>			Eastern Hemlock	
size factor, C <sub>F</sub> for compression		1.10		F <sub>b</sub> , F <sub>c</sub>	19%	0.8	0.7			Hem-Fir	
wet service factor, $\mathbf{C}_{\mathrm{M}}$ for bending		1.00		E	any	0.9	0.9			Hem-Fir (north)	
wet service factor, $C_{\ensuremath{M}}$ for compr	ression	1.00								Red Oak	
wet service factor, $C_{\ensuremath{M}}$ , for M. of	elasticity	1.00								Redwood	
temperature factor, C <sub>t</sub> , bending & compres. temperature factor, C <sub>t</sub> , for M. of elasticity			1.00 Southin Pine   1.00 Spruce,Pine,Fir								
									Spruce,Pine,Fir		
incised factor, C <sub>i</sub> , bending and c	compres.	1.00								Westn Cedar	
incised factor, C <sub>i</sub> , for M. of elast	ticity	1.00									
flat use factor, C <sub>fu</sub>		1.15				Size Factors, 0	C <sub>F</sub> for 2" and 4" I	lumber (f	or timbe	rs see formulas)	
repetitive member factor, Cr		1.00		Grade	Select Str	ructural, No. 1, No.	2, No. 3				
buckling stiffness factor, $C_T$		1.00		width	2,3	4	5	6	8	10	
SHAPE AND SUPPORT PARA	METERS			for F <sub>b</sub>	1.5	1.5	1.4	1.3	1.2	1.1	
section width, b =	3	inches		for F <sub>c</sub>	1.15	1.15	1.1	1.1	1.05	1	
section depth, d =	6	inches				-		-			
lateral support spacing, $L_U =$	32	inches			Flat Use Fa	actors, C <sub>fu</sub>					
				Width	2,3	4	5	6	8	10 and wider	
L <sub>II</sub> /d = 5.33				2" and 3" thick	1	1.1	1.1	1.15	1.15	1.2	
Effective bending length, Le =	65.9	inches		4" thick	-	1	1.05	1.05	1.05	1.1	
K <sub>bE</sub> =	0.439										
E =	1600000	psi			Effective Bendir	ng Length, L <sub>e</sub>					
R	2	• •		beam type	load type/location	when Lu/d < 7	when Lu/d 7	1			

$R_b =$	6.63			
$F_{bE} =$	15990			
$F_{b}=$		900	psi	
$F_b^*=$	1170			
C <sub>L</sub> =	0.995	F <sub>b1</sub> ' =	1165	psi
COLUM	N PARAMETERS	F <sub>b2</sub> ' =	1345	psi
K <sub>e major</sub> =		1.00		
K <sub>e minor</sub> =		0.80		
C =		0.80		
K <sub>cE</sub> =		0.30		
L <sub>e1</sub> =		96	inches	
L <sub>e2</sub> =		32	inches	
Q =	16.00			
$F_{cE} =$	1875			
$F_c =$		1350	psi	
F <sub>c</sub> *=	1485	psi		
J =	1.41			
C <sub>p</sub> =	0.765	F <sub>c</sub> '=	1135	psi
F <sub>cE1</sub> =	1875		f <sub>c</sub> =	
$F_{cE2} =$	4220		f <sub>b1</sub> =	
			f <sub>b2</sub> =	
I =	0.767	1.00		

design is O.K

Effective Bending Length, Le					
beam type	load type/location	when Lu/d < 7	when Lu/d 7		
cantilever	uniformly distributed	Le = 1.33Lu	Le = .90Lu + 3d		
cantilever	concentrated at unsupported end	Le = 1.87 Lu	Le = 1.44Lu + 3d		
cantilever	other	Le = 2.06 Lu	see note below*		
single span	uniformly distributed	Le = 2.06 Lu	Le = 1.63Lu + 36		
single span	conc. load & no lat- eral support at center	Le = 1.80 Lu	Le = 1.37Lu + 3d		
single span	conc. load & lateral support at center	Le = 1.11 Lu	Le = 1.11 Lu		
single span	conc. load & lateral support at 1/3 pts	Le = 1.68 Lu	Le = 1.68 Lu		
single span	conc. load & lateral support at 1/4 pts	Le = 1.54 Lu	Le = 1.54 Lu		
single span	conc. load & lateral support at 1/5 pts	Le = 1.68 Lu	Le = 1.68 Lu		
single span	conc. load & lateral support at 1/6 pts	Le = 1.73 Lu	Le = 1.73 Lu		
single span	conc. load & lateral support at 1/7 pts	Le = 1.78 Lu	Le = 1.78 Lu		
single span	7 conc. loads & lateral supports	Le = 1.84 Lu	Le = 1.84 Lu		
single span	equal end moments	Le = 1.84 Lu	Le = 1.84 Lu		
single span	other incl eccentric	Le = 2.06 Lu	see note below*		
multiple span	as single span or				

## engineering analysis when 7 Lu/d 14.3 Le = 1.63Lu + 3d when Lu/d >14.3 Le = 1.84 Lu



This spreadsheet is provided for illustrative teaching purposes only, and is not intended for use in any specific project. Anyone making use of the information contained in this spreadsheet does so at his/her own risk and assumes any and all resulting liability arising therefrom.

56 533 267